REDUNDANCY

It is often true, then, that at some point higher order interactions tend to

considering what effects can be estimated using only a half-fraction of a 25 studied. Fractional factorial designs exploit this redundancy. We begin by can be estimated and sometimes in an excess number of variables that are some have no distinguishable effects at all. We can encompass both is not small-redundancy in terms of an excess number of interactions that large number of variables is introduced into a design, it often happens that become negligible and can properly be disregarded. Also, when a moderately these ideas by saying that there tends to be redundancy in a 2^k design if kfactorial design.

P (%) 98.4 46.8 40.3 33.9 27.4 59.7 53.2 86.1 72.6 79.0 85.5 8.1 8 ယ္ 5 3 엉ŀ

FIGURE 12.1. (a) Normal plot of effects from 25 factorial design, reactor example

at Two Levels Fractional Factorial Designs

be generated and discusses their advantages and limitations. desired information can often be obtained by performing only a fraction of metrically as k is increased. It turns out, however, that when k is not small the The number of runs required by a full 2^k factorial design increases geothe full factorial design. This chapter describes how suitable fractions can

12.1. REDUNDANCY

ment requires $2^7 = 128$ runs. From these runs 128 statistics can be calculated which estimate the following effects: Consider a two-level design in seven variables. A complete factorial arrange-

| | average effects 2 | |
|----|---|------------------|
| 7 | effects | B ain |
| 21 | 2-factor | |
| 35 | 3-factor | |
| 35 | 4-factor | intera |
| 21 | 5-factor | interactions |
| 7 | 2-factor 3-factor 4-factor 5-factor 6-factor 7-factor | |
| - | 7-facto | |

of a response function. Ignoring, say, three-factor interactions corresponds all are of appreciable size. There tends to be a certain hierarchy. In terms of to ignoring terms of third order in the Taylor expansion.) and interactions can be associated with the terms of a Taylor series expansion discussed earlier. (In particular, for quantitative variables the main effects so on. This fact relates directly to the properties of smoothness and similarity actions, which in turn tend to be larger than three-factor interactions, and absolute magnitude, main effects tend to be larger than two-factor inter-Now the fact that all these effects can be estimated does not imply that they

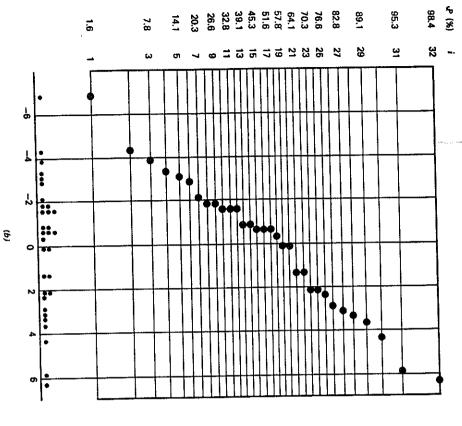


FIGURE 12.1. (b) Normal plot of residuals after eliminating 2, 4, 5, 24, and 45 from 2^5 factorial design, reactor example.

12.2. A HALF-FRACTION OF A 2^s DESIGN: REACTOR EXAMPLE

Table 12.1a shows data from a complete 2^5 factorial design analyzed in Table 12.1b. Normal plots (Figure 12.1) indicate that over the ranges of the variables studied the main effects 2, 4, and 5 and interactions 24 and 45 are the only effects distinguishable from noise.

a half-fraction of a 25 design: reactor example

TABLE 12.1a. Results from 2⁵ factorial design, reactor example

| | • | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----------------|-----------|----------------|----|----|-----|------------|----|-----|-----|--------------|-----|----|-----|-----|-------------|-----|----|----|----------|----------|----|----|----|----|----------|------------|----|------------|------------|----------|--------|----------|--------|-----------|----------|----------|-------|
| 30 31 *32 | 28 *29 | *26 | 25 | 24 | *23 | *22 | 21 | *20 | 19 | ~ | *17 | 16 | *15 | *14 | 13 . | *12 | = | 10 | * | * | 7 | 6 | *5 | 4 | ٿ | *2 | | run | | | un . | 4 | ω ı | . — | ۱۰ | | |
| + 1 + | + | + | l | 4- | ŀ | + | 1 | + | ļ · | + | i | + | 1 | + | ı | + | ı | + | ı | + | 1 | + | ı | + | ţ | + | 1 |) — | 1 | | conce | emp | agitat | feed r | | | |
| ++1 | 1 + + | - 1 | J | + | + | | | + | | | ı | + | + | 1 | ı | + | + | i | ı | + | + | 1 | i | + | + | 1 | ı | 2 | | 5 | ntrat | ratu | jon r | ate (| | variable | |
| +++ | + 1 1 | . 1 | ī | + | + | + | + | ı | 1 | I | Į | + | + | + | + | 1 | 1 | Į | ŀ | + | + | + | + | 1 | ŀ | i | 1 | , tus | | variable | tion (| ٦ - | ate (1 | iters/ | <u> </u> | ble | 318 |
| +++ | +++ | + + | + | ι | 1 | ķ | 1 | ı | 1 | 1 | I | + | + | + | + | + | + | + | + | i | ı | , | l | ١ | l | i | 1 | 4 | | ē | 8, | . و | (mgr) | ters/min) | | | 1,100 |
| +++ | +++ | + + | + | + | +. | + | + | + | + | + | + | ı | ļ | ı | l | ı | I | ı | 1 | l | ı | 1 | I | ļ | 1 | ļ | i | Ju | | | | | | | | | 3 |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | G | | w | 46 | 8 | _ = | 5 | I | |
| 81 82 | \$ 4 7 | 2 & | 4 | દ | 67 | <u>5</u> 5 | 59 | 65 | 70 | ස | 56 | 98 | 95 | 8 | 66 | 93 | 94 | 61 | 69 | 61 | 54 | 56 | 53 | 61 | ස | 5 3 | 61 | ٧ | % reacted) | response | 6 | 180 | 120 | 2 5 | 1, | + | Pro |

TABLE 12.1b. Analysis of 2⁵ factorial design, reactor example

estimates of effects

| | 45 = -11.0 | 35 = 0.875 | II | 25 = 2.0 | 24 = 13.25 | 23 = 0.875 | IJ | U | 13 = 0.75 | 12 = 1.375 | | 5 = -6.25 | 4 = 10.75 | 3 = -0.625 | 2 = 19.5 | I = -1.375 | average == 65.5 | |
|---------------|------------|------------|----|----------|------------|------------|-------------|--------------|-------------|------------|----|-----------|-----------|------------|----------|------------|-----------------|--|
| 12345 = -0.25 | 1345 = 1.0 | 1235 = 1.5 | 11 | 11 | n | | 345 = 0.125 | 245 = -0.250 | 234 = 1.125 | II | li | H L | 1 | ll I | | 123 = 1.50 | | |

The full 25 factorial requires 32 runs. Suppose that the experimenter had chosen to make only the 16 runs marked with asterisks in Table 12.1, so that only the data of Table 12.2 were available. When the 15 main effects and two-factor interactions are calculated from the reduced set of data in Table 12.2, they produce the estimates listed there, which are not very different from those obtained from the complete factorial design. Furthermore the normal plots of Figure 12.2 call attention to precisely the same effects: 2, 4, 24, 45 and 5. Thus the essential information could have been obtained with only half the effort.

The 16-run design in Table 12.2 is called a half-fraction. It is often designated as a 2^{5-1} fractional factorial design since

$$\frac{1}{2}2^5 = 2^{-1}2^5 = 2^52^{-1} = 2^{5-1}$$

The notation tells us that the design accommodates five variables, each at two levels, but that only $2^{5-1} = 2^4 = 16$ runs are employed.

TABLE 12.2 Analysis of a half-fraction of the full 2⁵ design: a 2⁵⁻¹ fractional factorial design, reactor example

| 17 2 2 3 20 5 5 22 22 23 23 23 24 25 27 27 27 27 27 27 27 27 27 27 27 27 27 | run |
|---|--|
| + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 | - |
| ++11++11++11++11 | 2 |
| ++++1111++++11111 | design |
| +++++++ | 4 5 4 3 2 1 |
| + + + + + + + + | ज इस के स |
| + + + + + + + + + + | variable rate (liters/min) talyst (%) itation rate (rpm) imperature (°C) ncentration (%) 12 13 14 15 |
| ++111++++111++ |) 10 1 100 140 3 3 |
| + + + + + + + + | 15 15 2 120 180 6 |
| + + + + + + + | - 5 |
| 55 55 55 55 55 55 55 55 55 55 55 55 55 | response (% reacted) |

estimates of effects

(assuming that three-factor and higher order interactions are negligible)

| | | | | 5 = -6.25 | 4 = 12.25 | 3 = 0.0 | 2 = 20.5 | l = -2.0 | average = 65.25 |
|------|------|------|------|-----------|-----------|---------|----------|----------|-----------------|
| H | 35 = | H | Il | U | 23 = | I | 14 = -1 | 13 == 1 | 12 = |
| 9.50 | 2.25 | 0.25 | 1.25 | 0.75 | 1.50 | 1.25 | 0.75 | 0.5 | 1.5 |

P (%)

96.7

90.0

83.3

76.7

70.0

63.3

56.7

50.0

43.3

36.7

30.0

23.3

16.7

10.0

3.3

į

15

14

13

12

11

10

9

8

7

6

5

4

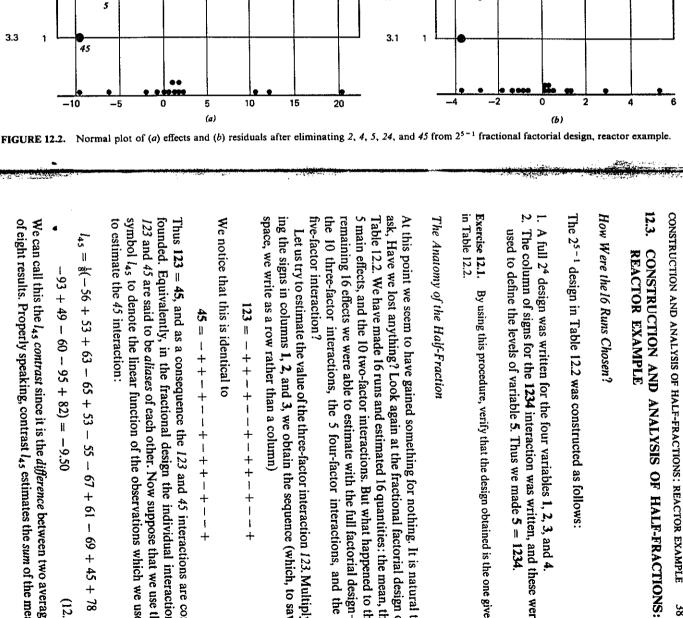
3

2

1

-10

381



How Were the 16 Runs Chosen?

The 25-1 design in Table 12.2 was constructed as follows:

ō

(b)

2

A full 24 design was written for the four variables 1, 2, 3, and 4. used to define the levels of variable 5. Thus we made 5 = 1234. The column of signs for the 1234 interaction was written, and these were

in Table 12.2. Exercise 12.1. By using this procedure, verify that the design obtained is the one given

The Anatomy of the Half-Fraction

i

16

15

14

13

12

11

10

9

8

7

6

5

4

3

2

P (%)

96.9

90.6

84.4

78.1

71.9

65.6

59.4

53.1

46.9

40.6

34.4

28.1

21.9

15.6

9.4

3.1

2

24

10

5

(a)

15

20

5 main effects, and the 10 two-factor interactions. But what happened to the ask, Have we lost anything? Look again at the fractional factorial design of At this point we seem to have gained something for nothing. It is natural to nve-factor interaction? the 10 three-factor interactions, the 5 four-factor interactions, and the remaining 16 effects we were able to estimate with the full factorial design-Table 12.2. We have made 16 runs and estimated 16 quantities: the mean, the

space, we write as a row rather than a column) ing the signs in columns 1, 2, and 3, we obtain the sequence (which, to save Let us try to estimate the value of the three-factor interaction 123. Multiply-

We notice that this is identical to

to estimate the 45 interaction: symbol l_{45} to denote the linear function of the observations which we used founded. Equivalently, in the fractional design the individual interactions Thus 123 = 45, and as a consequence the 123 and 45 interactions are con-123 and 45 are said to be aliases of each other. Now suppose that we use the

0

$$l_{45} = \frac{1}{8}(-56 + 53 + 63 - 65 + 53 - 55 - 67 + 61 - 69 + 45 + 78$$

-93 + 49 - 60 - 95 + 82) = -9.50 (12.1)

of eight results. Properly speaking, contrast l_{45} estimates the sum of the mean We can call this the l45 contrast since it is the difference between two averages

and five-factor interactions are obtained by multiplying signs, we get the values of effects 45 and 123. We indicate this by the notation $l_{45} \rightarrow 45 + 123$. results shown in Table 12.3. If the columns of signs corresponding to all the other three-factor, four-factor,

TABLE 12.3. Confounding pattern and estimates from 2^{s-1} design of Table 12.2

are identical. Verify the identity of the other column pairs in Table 12.3. Exercise 12.2. As was done for columns 45 and 123, verify that columns 24 and 135

A Justification for the Analysis

apparently justified. We shall see later that the analysis could also be justified effects of third and fourth order (represented by three-factor and four-factor Evidently our earlier analysis would be justified if it could be assumed that on different and somewhat more subtle grounds (see the subsection entitled interactions) could be ignored. In the reactor example the assumption was Experiment") "An Alternative Rationale for the Half-Fraction Design in the Reactor

How to Find the Confounding Patterns

sign sequences is extremely tedious. Fortunately a much more expeditious confounding pattern for any given design. The method of associating like route is available. To understand it remember the following four points: In manipulating fractional factorials it is important to be able to obtain the

- 1. Boldface numerals (e.g., 3 and 12) refer to columns of plus and minus
- 2. A product column is obtained by multiplication of the individual elements in the columns that make up that product. (The product column 124, for corresponding columns, 1, 2, and 4.) instance, is obtained by multiplication of the individual elements in the
- Multiplying the elements in any column by a column of identical elements gives a column of plus signs, which is designated by the letter I, that is,
- 4. A contrast like l_{45} in Equation 12.1 is obtained by multiplying the obser- $1 \times 1 = 1^2 = I$, $2^2 = I$, $3^2 = I$, $4^2 = I$, and so forth.
- quantity l is thus a contrast between two averages, each of N/2 observaby N/2 = 8 where N is the number of observations (16 in this case). Each vations by the appropriate plus and minus signs in column 45 and dividing observations by the column I of plus signs (i.e., summing the observations) tions. The single exception is $l_I = y$, which is obtained by multiplying the and dividing the result by N (in this example N = 16).

Generator and Defining Relation

The 25-1 design in Table 12.2 was constructed by setting

$$5 = 1234$$
 (12)

5, we obtain This relation is called the generator of the design. Multiplying both sides by

$$5 \times 5 = 1234 \times 5$$
 (12.3)

g

$$5^2 = 12345 \tag{12.4}$$

Thus the generator for the design can equivalently (and more conveniently)

be written as

$$I = 12345$$
 (12.)

elements in columns 1, 2, 3, 4, and 5, and noting that a column of plus signs, This version of the identity is readily confirmed by multiplying together the

385

I, is actually obtained. The half-fraction is defined* by a single generator, so that the relation I = 12345 also provides the *defining relation* of the design. This defining relation is the key to the confounding pattern. For example,

multiplying the defining relation on both sides by 1 yields

$$1 = 2345$$

In a similar way multiplying by 2 gives 2 = 1345 and so on to produce all the identities in the first column of Table 12.3.

The Complementary Half-Fraction

In the above example the generator 5 = 1234, or, equivalently, I = 12345, produced the defining relation for the design. In other words, by generating a new column 5 = 1234 we obtained the half-fraction corresponding to the runs marked with asterisks in Table 12.1. The defining relation I = 12345 provided by this generator immediately yields the confounding pattern of provided to the complementary half-fraction is generated by putting 5 = -1234. We then obtain the half-fraction corresponding to the runs of the original 2^5 that are not marked with asterisks in Table 12.1. The defining relation for this design may be written as

$$1 = -12345$$

In practice either half-fraction can equally well be used. For the data of Table 12.1 the complementary half-fraction would have given, for example,

$$l'_1 = -0.75 \rightarrow l - 2345$$

 $l'_2 = 18.50 \rightarrow 2 - 1345$

Exercise 12.3. For the 16 runs in Table 12.1 that do not have asterisks, calculate the average and the 15 contrasts $l'_1, l'_2, \ldots, l'_{45}$. Show by making a normal plot that the conclusions that would result from this fraction would be similar to those obtained from the other one.

Answer: (average, 1, 2, 3, 4, 5, 12, 13, 14, 15, 23, 24, 25, 34, 35, 45) = (65.75,
$$-0.75$$
, 18.5, -1.25 , 9.25, -6.25 , 1.25, 1.0, -1.0 , -1.0 , 0.25, 15.75, 2.75, 4.0, -0.5 , -12.5).

Combining the Two Half-Fractions

Suppose that after completing one of the half-fractions the other was subsequently added, so that the whole factorial was available. Unconfounded estimates of all effects

* When higher fractions are employed, there is more than one generator. For example, a quarter-fraction is defined by two generators. For more complicated fractions see Appendix 12A.

could then be obtained by analyzing the 32 runs as a full 25 factorial design run in two blocks of 16. The same result would be obtained by suitably adding and subtracting estimates from the two individual fractions. For example, we have

THE CONCEPT OF DESIGN RESOLUTION: REACTOR EXAMPLE

first fraction second fraction
$$l_2 = 20.5 \rightarrow 2 + 1345 \qquad l_2' = 18.5 \rightarrow 2 - 1345$$

whence

$$\frac{1}{2}(l_2 + l_3') = \frac{1}{2}(20.5 + 18.5) = 19.5 \to 2$$

$$\frac{1}{2}(l_2 - l_3') = \frac{1}{2}(20.5 - 18.5) = 1.0 \to 1345$$
(12.6)

These values for 2 and 1345 agree with those given in Table 12.1 for the complete 2⁵ design.

12.4. THE CONCEPT OF DESIGN RESOLUTION: REACTOR EXAMPLE

The 2^{5-1} fraction is called a *resolution V* design. Looking at the confounding pattern in Table 12.3, we see, for example, that $l_1 \rightarrow l + 2345$ and $l_{12} \rightarrow l2 + 345$. Thus main effects are confounded with four-factor interactions, and two-factor interactions with three-factor interactions.

In general, a design of resolution R is one in which no p-factor effect is confounded with any other effect containing less than R - p factors. The resolution of a design is denoted by the appropriate Roman letter appended as a subscript. Thus we could refer to the design of Table 12.2 as a 2^{p-1} design.

- 1. A design of resolution R = III does not confound main effects with one another but does confound main effects with two-factor interactions.
- 2. A design of resolution R = IV does not confound main effects and two-factor interactions but does confound two-factor interactions with other two-factor interactions.
- 3. A design of resolution R = V does not confound main effects and two-factor interactions with each other, but does confound two-factor interactions with three-factor interactions, and so on.

In general, the resolution of a two-level fractional design is the length of the shortest word in the defining relation.

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Resolutions of Some Half-Fractions

 2^{4-1} fractions with defining relations $I = \pm 1234$ have resolution IV. half-fractions with defining relations $I=\pm 123$ have resolution III, and the defining relation $I = \pm 12345$ has resolution V. In Table 12.4 the 2^{3-1} relation denotes the resolution of the design. Thus a 25-1 half-fraction with For any half-fraction the number of symbols on the right of the defining

Half-Fractions of Highest Resolution

effect column to accommodate the fifth variable. The choice we made yields a 25-1 design. In fact, it would have been possible to use any interaction or main At the beginning of Section 12.3 we gave a procedure for constructing a 2k-1 fractional factorial design of highest possible resolution: half-fraction with highest possible resolution. In general, to construct a

- 1. Write a full factorial design for the first k-1 variables.
- Associate the kth variable with plus or minus the interaction column 123...(k-1).

metrically in Table 12.4. Table 12.4 gives examples of 2_{HI}^{3-1} , 2_{IV}^{4-1} , and 2_{V}^{5-1} half-fractions of this kind. The two 23-1 half-fractions obtained by the above rule are shown geo-

5 = 123. Discuss its properties. What is its resolution? Can you imagine circumstances in which it might be preferred to the resolution V design? Exercise 12.4. Obtain the confounding pattern for a 25-1 design generated by setting

Partial answer: $l_1 \rightarrow l + 235$, $l_2 \rightarrow 2 + 135$, R = IV

in the Reactor Experiment An Alternative Rationale for the Half-Fraction Design

and minus signs from this design, we have a complete factorial in variables Obviously (from its mode of construction), if we omit the fifth column of plus Consider the $2\xi^{-1}$ half-fraction with I = 12345 given in Tables 12.2 and 12.4 ing variables is obtained whichever column is omitted. We have already seen factorial in variables 2, 3, 4, and 5! Indeed, a complete factorial in the remain-1, 2, 3, and 4. But try omitting column 1 instead. There is now a complete variables will produce detectable effects and the other will be essentially An alternative justifying assumption is that at most only four of the five that three-factor, four-factor, and five-factor interactions could be ignored that the experimenter could justify the 25-1 half-fraction on the assumption

TABLE 12.4. Best half-fractions for k = 3, k = 4, and k =

THE CONCEPT OF DESIGN RESOLUTION: REACTOR EXAMPLE

(1 = -1233 = -12(1 = 123)23-1 4 = 1234 = -123= -1234(1 = -12345)5 = -12345 = 1234

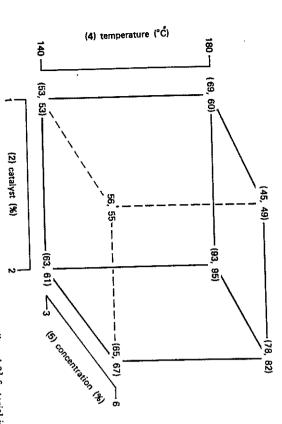
THE CONCEPT OF DESIGN RESOLUTION: REACTOR EXAMPLE

will generate complete factorials in the remaining variables, no matter which variables these are.

centration). Since variables 1 and 3 were effectively inert, we had a replicated variables had detectable effects: 2, 4, and 5 (catalyst, temperature, and con-23 factorial in variables 2, 4, and 5, and the results can be assembled as in In fact, our analysis for the reactor example suggests that only three of the

The General Importance of the Concept of Resolution Factorials Embedded in Fractions:

effective variables. This idea is illustrated with the 2^{3-1}_{11} design in Figure 12.4 and his conjecture is justified, he will have a complete factorial design in the contains complete factorials (possibly replicated) in every set of R -In general, it can be shown that a fractional factorial design of resolution R may have no detectable effects. Then, if he employs a design of resolution R variables but believes that all but R-1 of them (specific identity unknown) variables. Suppose, then, that the experimenter has a number of candidate which projects a 22 pattern in every subspace of two dimensions.



variables 2, 4, and 5, reactor example FIGURE 12.3. Data (% reacted) from a 25-1 fraction, shown as replicated 23 factorial in

FIGURE 12.4. A 2_{11}^{3} design, showing projections into three 2^2 factorials.

Exercise 12.5. If a resolution R design gives a full factorial in every set of R-1fewer than R-1 variables? variables, is it necessarily true that a full factorial is obtained in every subset containing Answer: Yes.

is the value of q? Exercise 12.6. A $2\sqrt[6]{-1}$ design gives full factorials in every subset of q variables. What Answer: 4, 3, 2, or 1 (for an example of q = 3 see Figure 12.3).

Sequential Use of Fractional Designs Economy in Experimentation Arising from the

Suppose that an experimenter who can make his runs sequentially wishes to containing 16 runs first, analyze the results, and think about them. If necessary, involving 32 runs. It is almost always better for him to run a half-fraction investigate five factors, each at two levels, and is contemplating a 25 design to the next stage of experimental iteration, which may involve, for example, he can always run the second fraction later to complete the full design. this sequential approach can thus greatly accelerate progress. It is worth the introduction of new variables or different levels of the old ones. Use of Frequently, however, the first half-fraction itself will allow him to proceed

1. The experimenter should randomize within each fraction.

2. If eventually it is decided to run both fractions, these fractions will be randomized orthogonal blocks of the complete design.

3. No information will be "lost" except that concerning the interaction which is actually confounded with the block contrast.

4. The design run as two randomized fractions can give greater precision than the whole design run in random order because the block difference is eliminated.

Recapitulation

We began the chapter by discussing redundancy. It was pointed out that, for moderate k, a full factorial design frequently makes possible the estimation of many more effects than are detectably different from the noise. Sometimes these nondetectable effects are high-order interactions and sometimes they are all the effects associated with some inert variable or variables.

The fractional factorials discussed in this chapter are ideally suited to exploiting the probable existence of redundancy of one or both of these kinds for the following reason:

It can be arranged so that the confounding that occurs is between effects
of high and low order.

of high and low order, 2. A complete factorial design is available for whichever subset of R-1 variables turns out to have appreciable effects.

In sequential experimentation, unless the total number of runs for a full or replicated factorial is needed to achieve sufficient precision, it is usually better to run fractional factorial designs. The fractions, used as building blocks, can build up to the full factorial design if this is necessary.

We now illustrate these ideas for designs of resolution III.

RESOLUTION III DESIGNS: BICYCLE EXAMPLE*

Suppose that the hypothetical data of Table 12.5 are times in seconds for a particular person to complete eight trial bicycle runs up a hill between fixed marks. These runs were performed in random order on eight successive days. The design is of resolution III and is a $\frac{18}{128} = \frac{1}{16}$ fraction of the full 2⁷ factorial. Thus it is a $2\frac{7}{10}$ design. (Note that $2^{7-4} = 2^72^{-4} = 2^{-4}2^7 = \frac{1}{16}2^7$.)

Table 12.6 gives the calculated contrasts. For example

$$l_1 = \frac{1}{2}(-69 + 52 - 60 + 83 - 71 + 50 - 59 + 88)$$
 (12.7)

 This hypothetical example is an extension of the real one in Appendix 11A, but it is assumed now that both the rider and the bicycle are different.

TABLE 12.5. An eight-run experimental design for studying how time to cycle up a hill is affected by seven variables (I = 124, I = 135, I = 236, I = 1237).

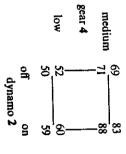
| run | seat up/down 1 | dynamo off/on 2 | handlebars up/down 3 | gear low/medium 4 12 | raincoat on/off 5 13 | breakfast yes/no 6 23 | tires hard/soft 7 123 | time to climb hill (sec) y |
|-----|----------------------|-----------------------|----------------------------|-------------------------------|-------------------------------|--------------------------------|--------------------------------|-------------------------------------|
| | | | | | + | + | | 69 |
| 1 | _ | | _ | <u>.</u> | <u>`</u> | + | + | 52 |
| 2 | + | | _ | | + | <u>-</u> | + | 60 |
| 3 | _ | + | _ | | T | _ | <u>-</u> | 83 |
| 4 | + | + | _ | + | _ | | _ | 71 |
| 5 | _ | | + | + | - | _ | -T- | 50 |
| 6 | + | | + | | + | - | | 59 |
| 7 | _ | + | + | | _ | + | | |
| 8 | + | + | + | + | + | + | + | 88 |

RESOLUTION III DESIGNS: BICYCLE EXAMPLE

TABLE 126.

Calculated contrasts and abbredata and design in Table 12.5 viated confounding pattern for

| | tires | breakfast | raincoat | gear | handlebars | dynamo | seat |
|------------------------------------|--|--|--|---|--|---|--|
| $(l_1 = 66.5 \rightarrow average)$ | $l_7 = 2.5 \rightarrow 7 + 34 + 25 + 16$ | $l_6 = 1.0 \rightarrow 6 + 23 + 45 + 17$ | $l_5 = 0.5 \rightarrow 5 + 13 + 46 + 27$ | $l_4 = (22.5) \rightarrow 4 + 12 + 56 + 37$ | $l_3 = 1.0 \rightarrow 3 + 15 + 26 + 47$ | $l_2 = (12.0) \rightarrow 2 + 14 + 36 + 57$ | $I_1 = 3.5 \rightarrow 1 + 24 + 35 + 67$ |



culated effects l_1, l_2, \ldots, l_7 have a standard error of about actions between three or more factors have been ignored. Suppose that runs up the hill under the same conditions is about 3 seconds. Thus the calprevious experience suggested that the standard deviation for repeated The table also gives an abbreviated* confounding pattern in which inter-

$$\sqrt{\frac{3^2}{4} + \frac{3^2}{4}} = 2.1$$

is that only two of the seven factors, the dynamo (2) and gear (4), exert a deof low gear adds about 22 seconds. On this interpretation we have in effect dynamo on adds about 12 seconds to the time, and using medium gear instead tectable influence, and they do so by way of their main effects. Having the Their values are circled in Table 12.6. The simplest interpretation of the results Evidently only two contrasts, l_2 and l_4 , are distinguishable from noise.

of the nature of his bicycle suggests that the simpler explanation is likely to a replicated 22 design in the variables 2 and 4, as indicated at the bottom of the investigation at this point. possible, for example, that l_4 is large, not because of a large main effect 4, but be right. The experimenter might well decide to proceed to the next stage of However, for this example we suppose that the experimenter's knowledge Table 12.6. There is, of course, some ambiguity in these conclusions. It is 12B how sequential addition of further runs can resolve such ambiguities. because one or more of the interactions 12,56,37 are large. We see in Appendix

of each of the factors, assuming that they do not interact, these arrangements have sometimes been called "main effect plans." Because one use of resolution III designs is to determine the main effects

Embedded 22 Factorials in Resolution III designs

example, whichever two columns of the design are chosen, they form a 4, are effective, and the rest, that is, 1, 3, 5, 6, and 7, are essentially inert. confounding pattern in Table 12.6 supposing that two variables, say 2 and complete 22 factorial replicated twice. Also notice what happens to the subset of R-1 variables. For the resolution III design of Table 12.5, for A resolution R design has a complete factorial (possibly replicated) in every $l_2 \rightarrow 2$, $l_4 \rightarrow 4$, and $l_1 \rightarrow 24$, and the remaining I's measure experimental Then all interactions and main effects containing these numbers vanish,

from a design of resolution R produces a full factorial design Exercise 12.7. For the examples in Table 12.4, verify that any subset of R-1 variables

Construction of 2111 Design

The 27-4 design in Table 12.5 can be constructed as follows:

 Write a full factorial design for the three variables, 1, 2, and 3. Associate additional variables 4, 5, 6, and 7 with all the interaction columns 12, 13, 23, and 123, respectively.

and is therefore sometimes called a saturated design.* The design is obtained by associating every available contrast with a variable

[•] The method by which the confounding pattern has been obtained is given in Appendix 12A.

ordinary circumstances * It is actually possible to construct supersaturated designs, but we do not recommend them in

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In Table 12.5 a one-sixteenth fraction of a full 2⁷ factorial design is shown. How can the other one-sixteenth fractions that make up the full factorial design be generated? The first design was generated by setting

$$4 = +12$$
 $5 = +13$ $6 = +23$ $7 = +123$ (12.8)

but, for example, we could equally well have used

$$4 = -12$$
 $5 = +13$ $6 = +23$ $7 = +123$ (12.9)

This gives a different one-sixteenth fraction, which is shown in Table 12.7 with further hypothetical data on times to cycle up the hill. Note that none of the runs in this new design is the same as any of those in the preceding design. Calculated contrasts for this design are shown in Table 12.8.

TABLE 12.7. A second 2_{11}^{7-4} fractional factorial design with times to cycle up a hill (I = -124, I = 135, I = 236, I = 1,237).

| 10 11 13 14 15 | 를 |
|----------------------------|--------------------------------|
| + + + + | seat |
| ++11++11 | dyname 2 |
| ++++1111 | handlebars |
| 1++11++1 | gear 4 |
| + + + + | raincoat 5 |
| ++1111++ | |
| + 1 1 + 1 + + | tires |
| 53 53 56 60 | time to climb hill (sec) |

What is the confounding pattern for the new fraction? Notice that the new fraction was obtained by switching signs for variable 4 in the first design (variable 4 was associated with -12 instead of +12). The abbreviated confounding pattern for this new fraction may be obtained, therefore, by switching signs in the confounding pattern of Table 12.6. This gives the confounding pattern in Table 12.8.

For this set of data the contrasts calculated from the second fraction confirm the conclusions from the first fraction.

RESOLUTION III DESIGNS: BICYCLE EXAMPLE TABLE 12.8. Calculated contrasts and abbreviated confounding

pattern for second design in bicycle experiment

| $l_5' = -1.7 \rightarrow 5 + l3 - 46 + 27$ $l_6' = 2.2 \rightarrow 6 + 23 - 45 + l7$ $l_7' = -0.7 \rightarrow 7 - 34 + 25 + l6$ | | 1 | 11 | $l_2' = 10.2 \rightarrow 2 - 14 + 36 + 57$ | 11 |
|---|-------------------|---|----|--|----|
| | 4 + 12 + | 1 | | | |
| | -4 + 12 + 56 + 37 | | | | |
| | | | | | |

The Sixteen Different Fractions

In all there are 16 different ways of allocating signs to the four generators:

$$4 = \pm 12$$
, $5 = \pm 13$, $6 = \pm 23$, $7 = \pm 123$ (12.1)

Thus appropriate sign switching in columns* 4, 5, 6, and 7 of Table 12.5 produces 16 fractional factorial designs which together make up the complete 2⁷ factorial design. Corresponding sign switching in Table 12.6 produces the 16 different confounding patterns.

Designing Two Fractions

Consider again the bicycle example. Suppose that the 16 results from the two 2_{11}^{7-4} fractionals were considered together. What conclusions could be drawn? Combining the results from Tables 12.6 and 12.8, we obtain Table 12.9

Conclusions would now be somewhat more certain. In particular, the large main effect of factor 4 (gear) is now estimated free of bias from two-factor interactions, and has a value close to that conjectured earlier. The joint effect of the string of interactions 12 + 56 + 37 can now be estimated separately from the main effect 4, and it is shown to be small. Most interestingly, all the two-factor interactions involving the important variable 4 are now free of aliases. (Of course we continue to assume all three-factor and higher order interactions to be zero.) For this particular set of data, however, none of these two-factor interactions is distinguishable from noise. Factor 2 (dynamo), somewhat less aliased than before, is showing an effect similar to that previously conjectured.

^{*} The reader can confirm by experimentation that switching signs in other columns of the design only produces one or another of these basic 16 fractions. However, the *order* in which the runs appear can be different.

| | | tires | geal raincoat breakfast | handlebars | seat |
|--|-------|--|--|--|---|
| $ \frac{1}{3}(l_5 - l_5') = \frac{1}{3}(0.5 + 1.7) = 1.1 \rightarrow 46 $ $ \frac{1}{3}(l_6 - l_6') = \frac{1}{3}(1.0 - 2.2) = -0.6 \rightarrow 45 $ $ \frac{1}{3}(l_7 - l_7') = \frac{1}{3}(2.5 + 0.7) = 1.6 \rightarrow 34 $ | 1 1 1 | $+ l_1^2 = \frac{1}{2}(2.5 - 0.7)$ $- l_1^2 = \frac{1}{2}(3.5 - 0.8)$ | $+ \frac{1}{15} = \frac{1}{2}(0.5 - 1.7)$ $+ \frac{1}{15} = \frac{1}{2}(1.0 + 2.2)$ | $+ i_3' = \frac{1}{2}(1.0 + 2.7)$ + $i_3' = \frac{1}{2}(22.5 + 25.2)$ | $\frac{1}{2}(l_1 + l_1') = \frac{1}{2}(3.5 + 0.8) = 2.2 \rightarrow l + 35 + 67$ $\frac{1}{2}(l_1 + l_1') = \frac{1}{2}(12.0 + 10.2) = 11.1 \rightarrow 2 + 36 + 57$ |

Sequential Use of Highly Fractionated Designs

The preceding example illustrates a useful application of highly fractionated designs as sequential building blocks. Additional fractions may be selected to resolve ambiguities, which knowledge of the variables and data available so far suggest may be of importance. We explore two important applications of this idea. The reader can devise others to suit particular circumstances.

Addition of a Second Fraction to De-alias Any One Main Effect and All Its Associated Two-Factor Interactions

Consider the two fractions used in the bicycle experiment. The largest effect obtained from the first set of eight runs was associated with the choice of gear (variable 4). It might have been argued, therefore, that if further runs were to be made, they could best be employed to de-alias 4 and all the interactions of

other variables with 4.

Table 12.9 shows that by adding a second fraction in which the sign of variable 4 has been switched, a design of 16 runs possessing the desired property is obtained. This ability to de-alias one effect and all its two-factor interactions by adding a second fraction with the appropriate column of signs switched is a handy device for the sequential use of these designs.

Adding a Second Fraction to De-alias All Main Effects

Consider Table 12.5 again, and suppose that a different second fraction is added in which signs are switched in all the columns. Then for the new fraction

the first two rows in the confounding pattern (obtained by switching signs in Table 12.6) are

RESOLUTION III DESIGNS: BICYCLE EXAMPLE

$$l'_1 \rightarrow l - 24 - 35 - 67$$
 $(l'_{-1} \rightarrow -l + 24 + 35 + 67)$ (12.11 $l'_2 \rightarrow 2 - l4 - 36 - 57$ $(l'_{-2} \rightarrow -2 + l4 + 36 + 57)$

By combining this second fraction with the original fraction, we obtain

$$\frac{1}{2}(l_1 + l_1') \to l, \quad \frac{1}{2}(l_1 - l_1') \to 24 + 35 + 67$$

$$\frac{1}{2}(l_2 + l_2') \to 2, \quad \frac{1}{2}(l_2 - l_2') \to 14 + 36 + 57$$
(12.1)

and so on.

This way of augmenting the design yields all main effects clear of all two-factor interactions, but the two-factor interactions themselves are still confounded in groups of three. An example of the use of this sequence is given in Section 13.3.

Exercise 12.8. Show that the second fraction obtained above by switching all signs may also be obtained (with runs in a different order) by switching signs in columns 4, 5, 6, and 7 only. Can you find other ways to reproduce the second fraction? Explain the equivalences you find.

General Construction of Resolution III Designs

Resolution III designs for $2^k - 1$ variables may be obtained by saturating a 2^k factorial with additional variables. For example, to construct a saturated 16-run design in 15 variables first write a full factorial design for four variables and then associate the extra variables 5, 6, ..., 15 with the 11 interaction columns 12, 13, 14, 23, 24, 34, 123, 124, 134, 234, and 1234, respectively. The resulting design is a 2_{11}^{15} fractional factorial design for 15 variables in 16 runs.

Exercise 12.9. Construct a two-level fractional factorial design for 31 variables in 32 runs. This is a 2^{k-p} design; what values do k and p have? Answer: k = 31, p = 26.

Exercise 12.10. Indicate how you could construct a 263-57 fractional factorial design.

Answer: Yes.

Useful designs may be obtained by appropriately deleting columns from the saturated designs. For example, dropping columns 4 and 7 from the design matrix for a 2^{7-4} design yields a 2^{5-2} design, the defining relation for which can be obtained from that for the 2^{7-4} design by deleting all words containing 4 and 7. The variables to be dropped are selected so as to obtain the most satisfactory alias arrangement.

The saturated fractional factorial designs have the following orthogonal* property: if we take any two columns, then, corresponding to the N/2 plus signs in the first column, there will be N/4 plus and N/4 minus signs in the second column, and similarly for the minus signs in the first column. Provided that all interactions are negligible, designs with this property allow unbiased estimation of all main effects of N-1 variables with smallest possible variance. The fractional factorials so far discussed are available only if N is a power of 2. Plackett and Burman (1946) have obtained arrangements with this same orthogonal property when N is a multiple of 4. For example, their design for k=11 factors in N=12 runs is shown in Table 12.10. The fashion in which two-factor interactions confound main effects for most Plackett and Burman designs is complicated. However, fold-over pairs of any such orthogonal design are of resolution IV (see Box and Wilson, 1951).

TABLE 12.10. Plackett and Burman design for study of 11 factors in 12 runs

| | • | ٠ | ٠ | - | , | , ### | . 7 | 0 | • | 51 | |
|-----|---|---|---|---|---|---------|------------|----|----|----|---|
| run | - | N | Ĺ | 4 | 5 | 6 | 7 | ox | عا | ē | = |
| - | + | 1 | + | ı | 1 | ļ | + | + | + | 1 | |
| 2 | + | + | 1 | + | 1 | ļ | ı | + | + | + | |
| ιų | į | + | + | ŀ | + | i | 1 | 1 | + | + | |
| 4 | + | 1 | + | + | i | + | 1 | l | 1 | + | |
| Ų, | + | + | ł | + | + | i | + | 1 | 1 | ı | |
| 6 | + | + | + | I | + | + | j | + | 1 | ı | |
| 7 | ı | + | + | + | ļ | + | + | 1 | + | 1 | |
| œ | ı | 1 | + | + | + | ī | + | + | 1 | + | |
| 9 | į | ı | 1 | + | + | + | ı | + | + | 1 | |
| 0 | + | 1 | I | 1 | + | + | + | 1 | + | + | 1 |
| = | ı | + | 1 | ı | ı | + | + | + | ı | + | |
| 5 | 1 | l | l | į | l | ı | ı | 1 | ı | 1 | |

12.6. RESOLUTION IV DESIGNS: INJECTION MOLDING EXAMPLE

We have seen that for designs of resolution V main effects are confounded only with four-factor interactions, and two-factor interactions only with three-factor interactions. Full factorial designs are generated by every subset

RESOLUTION IV DESIGNS: INJECTION MOLDING EXAMPLE

of four variables. Designs of resolution III introduce much more serious confounding, with main effects having two-factor interactions as aliases. For these designs full factorial designs exist for every subset of two variables. Designs of resolution IV occupy an intermediate position. No main effect is confounded with any two-factor interaction, but two-factor interactions are confounded with each other. For these designs full factorial designs exist for every subset of three variables.

An Experiment on Injection Molding

choose a further fraction of eight or 16 runs designed to resolve the ambiguity most likely to explain the large size of l_{15} are perhaps 15 and 38, since these is shown in Table 12.12. It seems likely that main effects associated with shown in Figure 12.5, suggest that the linear contrasts l_3 , l_{15} , and l_5 are disin a $2_{\rm IV}^{8-4}$ (a $_{\rm Id}^{1}$ replicate of a 2^{8} factorial of resolution IV). The normal plots, In an injection molding experiment (Table 12.11) eight variables were studied further information the situation is uncertain. One way to proceed is to involve factors 3 and 5, which have large main effects. It is, however, possible holding pressure (3) and booster pressure (5) exist. Also, the interactions ing pattern, assuming negligible interaction between three or more factors, tinguishable from the noise. The largest remaining effect is l_{B} . The confoundand estimate the responsible interaction. problem might be resolved with even fewer than eight runs. We show in However, in this particular example the large size of l15 suggested that the Appendix 12B how four additional runs were chosen and used to discover that interactions exist between factors that have no main effects. Without

Construction of the Resolution IV Design by "Folding Over" a Resolution III Design

The sixteen-run 2_{11}^{8-4} design in Table 12.11 was constructed as follows. The eight-run 2_{11}^{7-4} design was first written as in Table 12.5 for the seven variables 1, 2, 3, ..., 7. A further column labeled 8 and consisting entirely of plus signs was then added. The remaining eight runs were obtained by switching all signs in the first set of eight runs. Thus run 9 was obtained by switching all signs in run 1 and so on.

The Alias Pattern

The alias pattern for the folded-over design given in Table 12.11 can be obtained from that of the resolution III design (Table 12.6) by the following argument. Suppose that we compute for the first set of eight runs

$$l_1 = \frac{1}{3}(-y_1 + y_2 \dots + y_8)$$

[•] If the level of the *i*th variable is represented by $x_i = \pm 1$ and that of the *j*th variable by $x_j = \pm 1$, then $\sum x_i = 0$, $\sum x_j = 0$, and $\sum x_i x_j = 0$ for every *i* and *j*.

and for the second set of eight runs

$$-l_1^{\prime} = \frac{1}{4}(-y_9 + y_{10} \cdots + y_{16})$$

Then using Table 12.6 $l_1 \rightarrow 1 + 18 + 24 + 35 + 67$

$$18 + 24 + 35 + 67$$
 and $-l_1' = -l + 18 + 24 + 35 + 67$

Now the contrast l_1 for the complete set of 16 runs is

$$l_1 = \frac{1}{8}(-y_1 + y_2 + \dots + y_8 + y_9 - y_{10} \dots - y_{16}) = \frac{1}{2}(l_1 + l_1')$$

333 90.0 50.0 56.7 63.3 96.7 23.3 30.0 36.7 70.0 76.7 Z 83 16.7 <u>5</u> ဋ္ဌ **=** 5 = 12 ដ 3 15 + 26 + 38 + 47

FIGURE 12.5. (a) Normal plot of contrasts, injection molding example.

Similarly for the contrast associated with the interaction 18 it is

RESOLUTION IV DESIGNS: INJECTION MOLDING EXAMPLE

 $l_{18} = \frac{1}{8}(-y_1 + y_2 + \cdots - y_8 - y_9 + y_{10} + \cdots + y_{16}) = \frac{1}{8}(l_1 - l_1).$

Thus $l_1 \rightarrow l$ and $l_{18} \rightarrow l8 + 24 + 35 + 67$. The same argument applied to

more complete discussion is given in Appendix 12A. the remaining contrasts yields the confounding pattern of Table 12.12. A

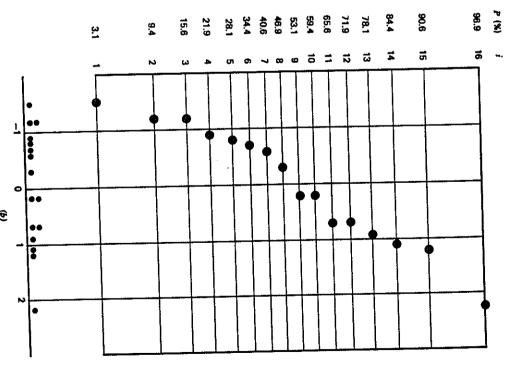


FIGURE 12.5. (b) Normal plot of residuals 2_{V}^{8-4} design, injection molding example.

| run | mold temperature | moisture content | holding pressure | cavity thickness | booster pressure | cycle time | gate size 7 | screw speed | shrinkage y |
|-----|---------------------|---------------------|---------------------|---------------------|---------------------|---------------|-------------------|----------------|----------------|
| | | | | | | | | | |
| 2 | + | _ | _ | | _ | + | + | + | 16.8 |
| 3 | _ | + | | _ | + | _ | + | + | 15.0 |
| 4 | + | + | | + | _ | _ | _ | + | 15.4 |
| 5 | · | | + | + | | _ | + | + | 27.6 |
| 6 | + | _ | + | _ | + | | _ | + | 24.0 |
| 7 | <u>.</u> | + | + | _ | | + | _ | + | 27.4 |
| 8 | + | + | + | + | + | + | + | + | 22.6 |
| 9 | + | <u>.</u> | + | <u>-</u> | _ | _ | + | | 22.3 |
| 10 | <u>.</u> | <u>.</u> | + | + | + | | | | 17.1 |
| 11 | + | | + | + | _ | + | | _ | 21.5 |
| 12 | _ | _ | + | - | + | + | + | _ | 17.5 |
| 13 | + | + | <u>.</u> | _ | + | + | _ | _ | 15.9 |
| 14 | • | + | _ | + | _ | + | + | | 21.9 |
| 15 | + | , — | _ | + | + | | + | _ | 16.7 |
| 16 | <u>.</u> | _ | | <u>-</u> | _ | | | - | 20.3 |

Alternative 28-4 Fractions

average =

18 + 24 + 35 + 67

sign switching. Exactly as with the resolution III designs, the switching of Sixteen different 2_{IV}^{8-4} fractions are members of the family making up the complete 2^8 design. Individual members of the family may be generated by signs in one or more columns will always yield a member of the family, and sign changes in the alias patterns of Table 12.12. the associated confounding pattern is obtained by making the corresponding

Building Blocks

confounding links. designs. As before, sign switching may be used to eliminate particular Resolution IV designs may be used sequentially as were the resolution III

General Construction of Resolution IV Designs

The construction of a resolution IV design containing 2^k variables follows exactly the pattern given for the $2_{\rm IV}^{8-4}$ design:

- Write a complete 2^k factorial with added columns for all interaction terms.
- Generate a resolution III design for $2^k 1$ variables by saturating this design with variables.
-). Add a further variable as a column of plus signs.
- 4. Repeat the design with all signs reversed to give a resolution IV design for 2^{k+1} runs.

An alternative general method is given in Appendix 12A.

12.7. ELIMINATION OF BLOCK EFFECTS IN FRACTIONAL DESIGNS

Fractional designs may be run in blocks, with suitable contrasts used as "block variables." A design in 29 blocks is defined by q independent contrasts. All effects (including aliases) associated with these basic contrasts and all their interactions are confounded with blocks.

Example 25⁻¹ Design in Two Blocks of Eight

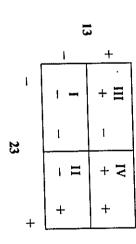
Consider again the 2^{5-1} design of Table 12.2. Suppose the investigator decided that interaction between feed rate and catalyst concentration was likely to be negligible. This interaction 13 could then be used for blocking. The eight runs 2, 20, 5, ..., 15, having a minus sign in the 13 column, would be run in one block, and the eight runs 17, 3, 22, ..., 32 in the other. Notice that in this design the alias 245 (here assumed negligible) of 13 is also confounded with blocks.

Example: 25-1 Design in Four Blocks of Four Runs

Suppose that, in the 2^{5-1} design of Table 12.2, columns 13 and 23 are confounded with blocks. Then the interaction between these columns $13 \times 23 = 12^2 = 12$ is also confounded. The design would thus be appropriate if we were prepared to confound with blocks all two-factor interactions between variables 1, 2, and 3 and their aliases. To achieve this arrangement, runs 20, 5, 12, and 29, for which the 13 and 23 columns have signs (--), could be put in the first block, runs 2, 23, 26, and 15, for which columns 13 and 23 have signs (-+) in the second block, and so on. Thus in terms of a two-way table the arrangement would be as follows:

ELIMINATION OF BLOCK EFFECTS IN FRACTIONAL DESIGNS

ζ,



The Resolution IV Designs as Main Effect Plans in Blocks of Two

investigation the subject of study was an effluent impurity that tended to provides economical main effect plans with a block size of only two. In one remarkable class of such designs based on the resolution IV arrangement It occasionally happens that we must work with very small block sizes. A vary slowly with time. Runs made consecutively were thus much more com l_{13} , to accommodate $\mathbf{B_2}$; then l_{17} cannot be used for $\mathbf{B_3}$ since it can be obstrings in Table 12.12. For the blocking scheme suppose that we use any twoblocked $2_{\rm N}^{8-4}$ design. The plan is shown in Table 12.13. To see how this is effect plan was used to study the main effects of eight variables based on a blocks of 2-hour periods, one experimental condition being run in the first parable than those made further apart. It was possible to run the design in tained by multiplying the signs of 12 and 13. Suppose, therefore, we use l_{14} derived, consider the original design given in Table 12.11 and the aliasing hour and one in the second. At one stage of the investigation a 16-run main spond to the contrasts l_{12} , l_{13} , l_{14} , l_{15} , l_{16} , l_{17} , l_{18} , in some order. They thus of signs obtained for B1, B2, B3, B1B2, B1B3, B2B3, B1B2B3 exactly correinteraction contrast can equally well be employed.) Then the seven columns for ${\bf B_3}$. (The reader may confirm that any other remaining two-factor factor interaction contrast, say l_{12} , to accommodate $\mathbf{B_1}$, and a second, say design is rearranged in the eight blocks as on the right of Table 12.13, it is seen involve only the strings of interactions and not the main effects. When the first run, that is, the signs in one run are exactly reversed in the other. that the second run in each block is the mirror image or "fold-over" of the

In designs of this kind, both the ordering within pairs and the sequence in which the pairs (blocks) are run should be random.

Rather than regard all between-block information as lost, the design can be analyzed on the basis that there are two different error variances. The within-block variance is appropriate for inferences about main effects, and the between-block variance for inferences about the strings of two-factor